

03 NATM



What means NATM

New

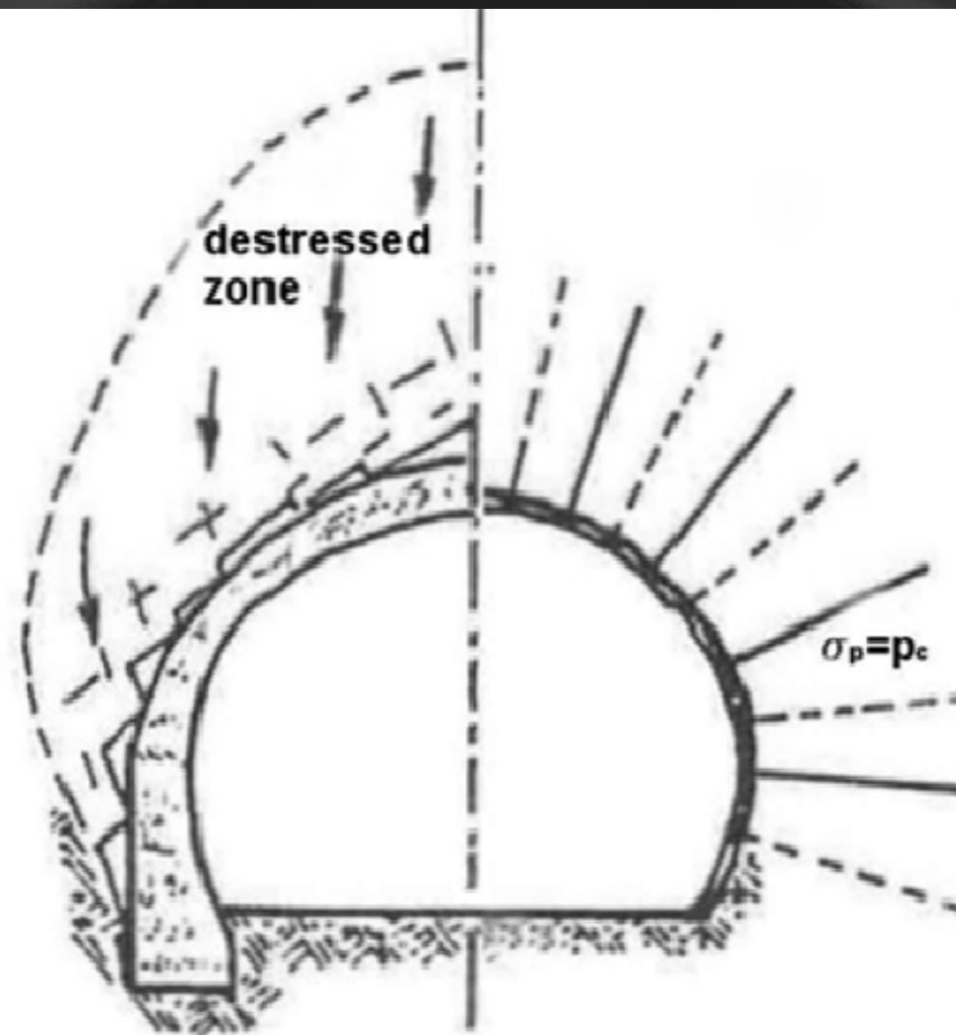
Austrian

Tunnel

Method

Not so new ...

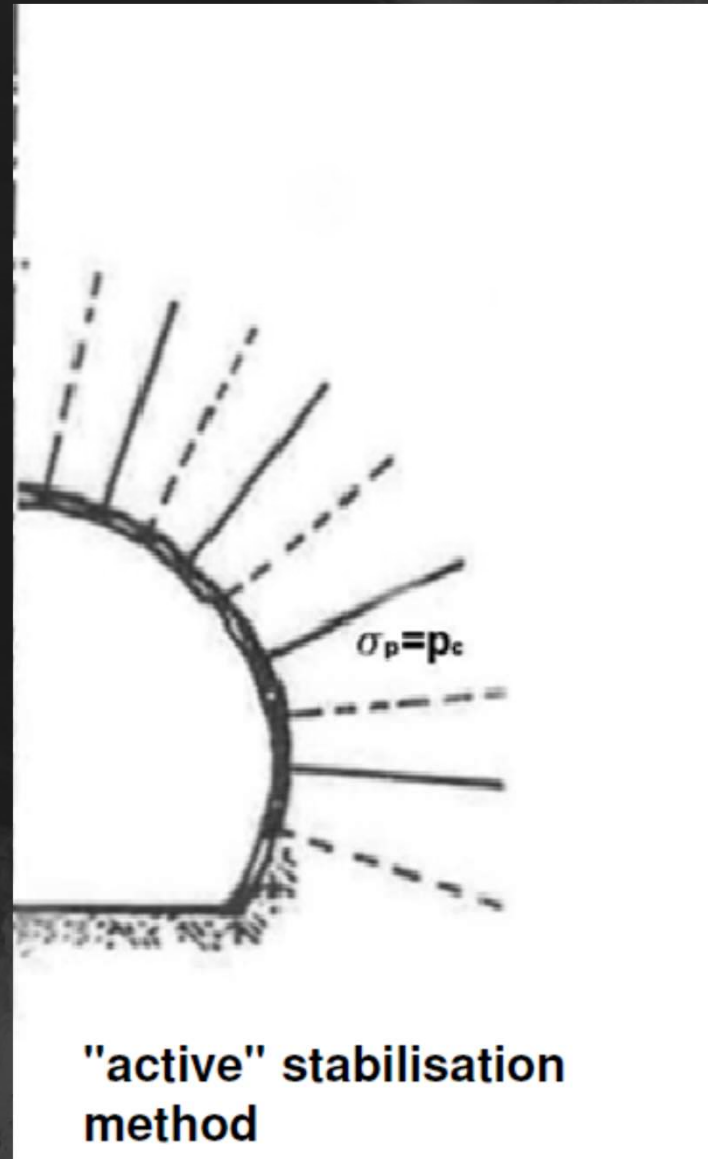
older than 50 y...



Traditional "passive"
method

"active" stabilisation
method

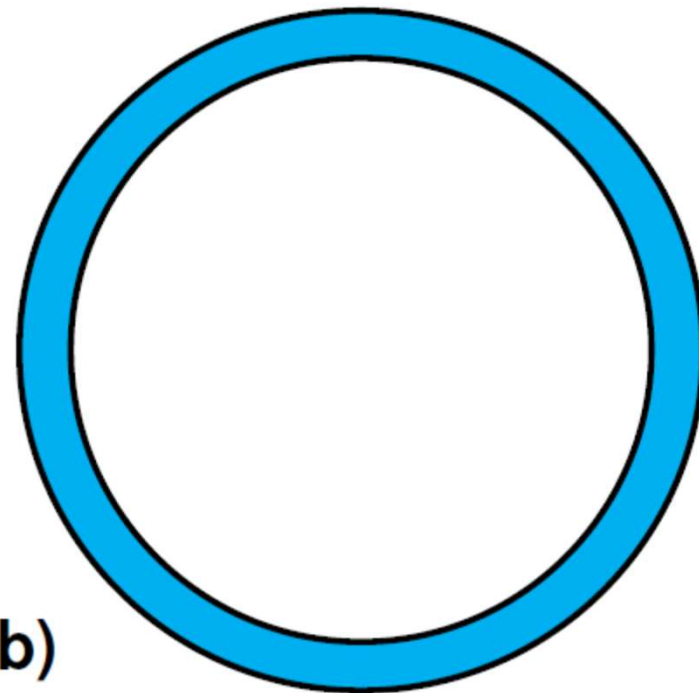
Main content of NATM is that a ring of rock around the excavated hole is requested to support some of the load coming from the overburden



Criteri progettuali limite per realizzare i sostegni

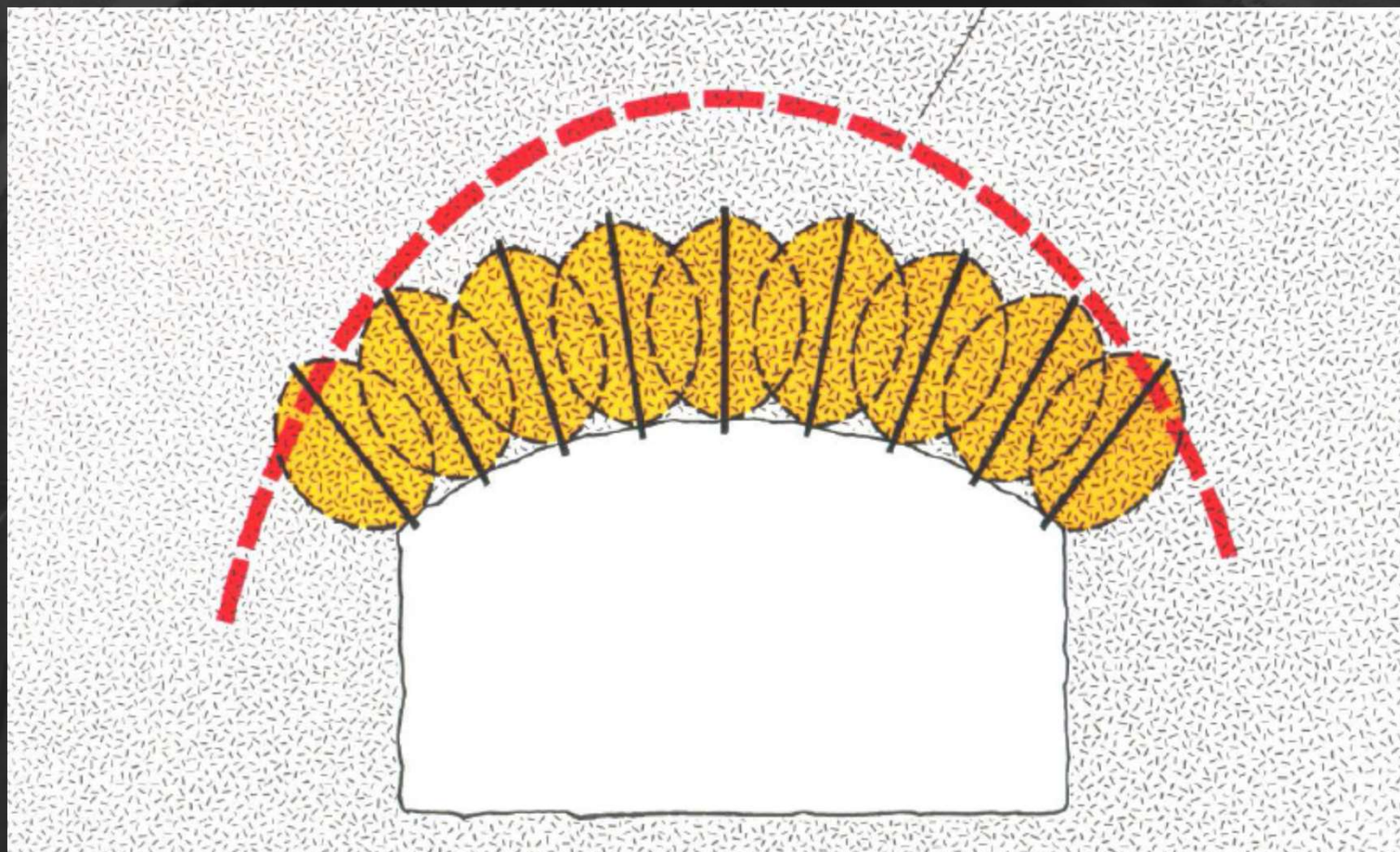


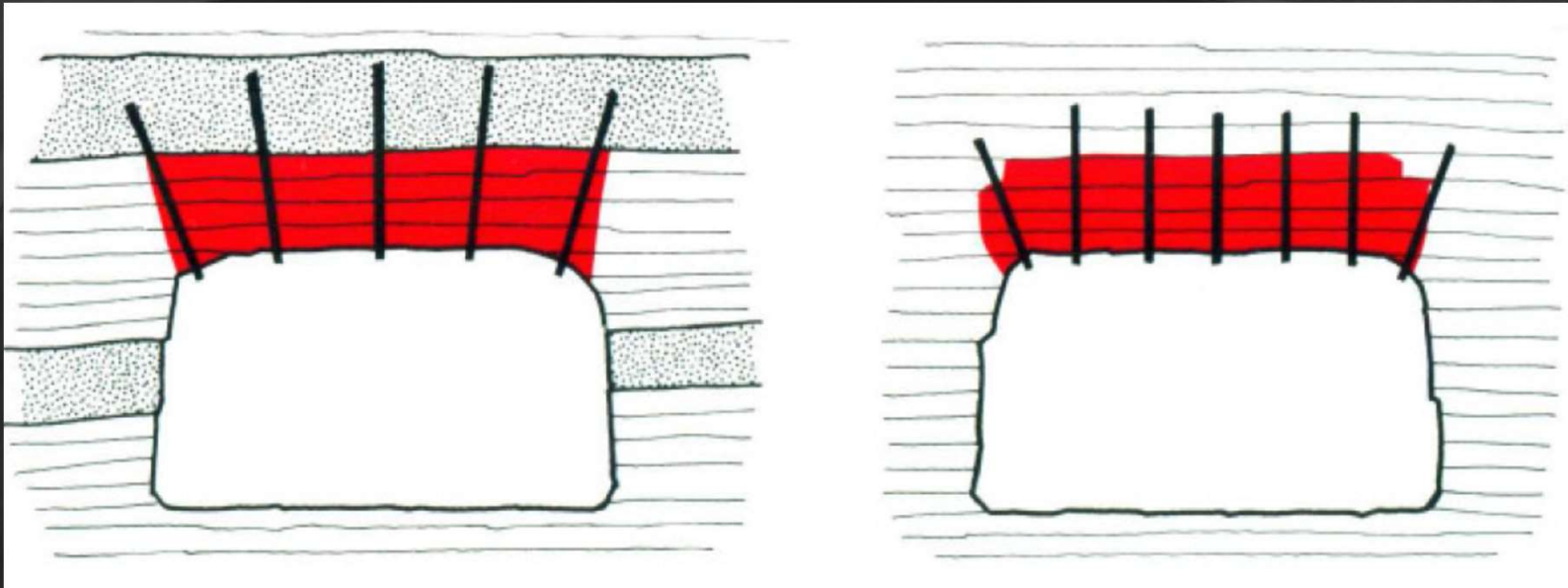
a)



b)

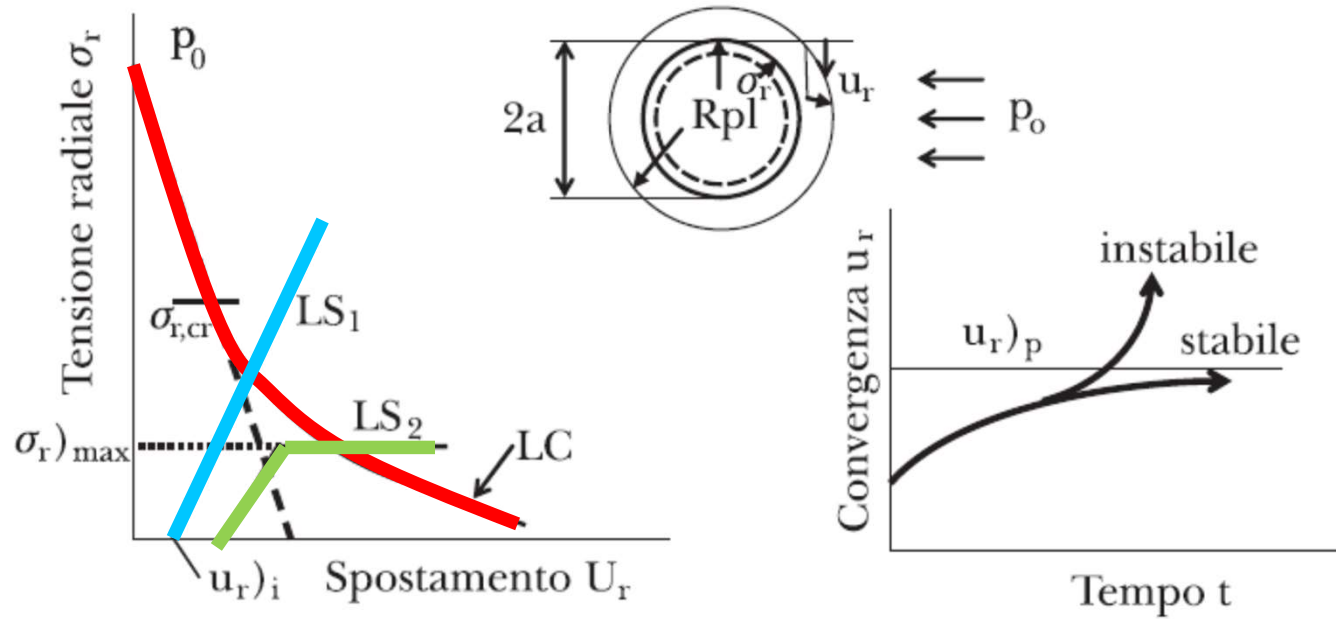
sovrascavo





I bulloni aumentano la rigidità degli strati rocciosi

LS_1 supporto "elastico" — $\downarrow \downarrow \downarrow$
 LS_2 supporto "cedevole" — $\downarrow \downarrow \downarrow$



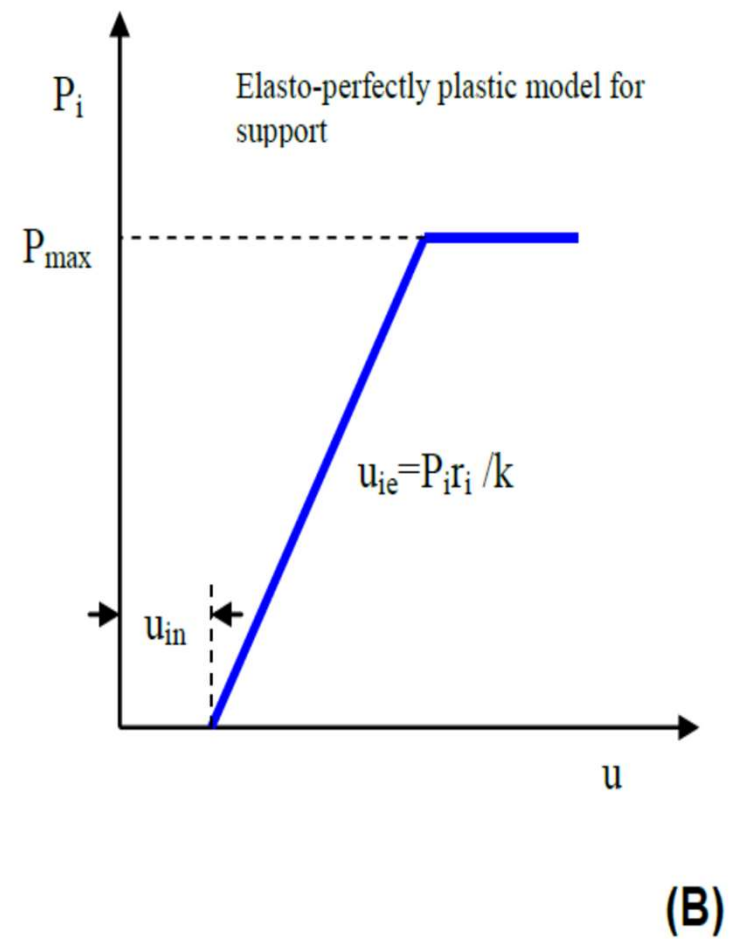
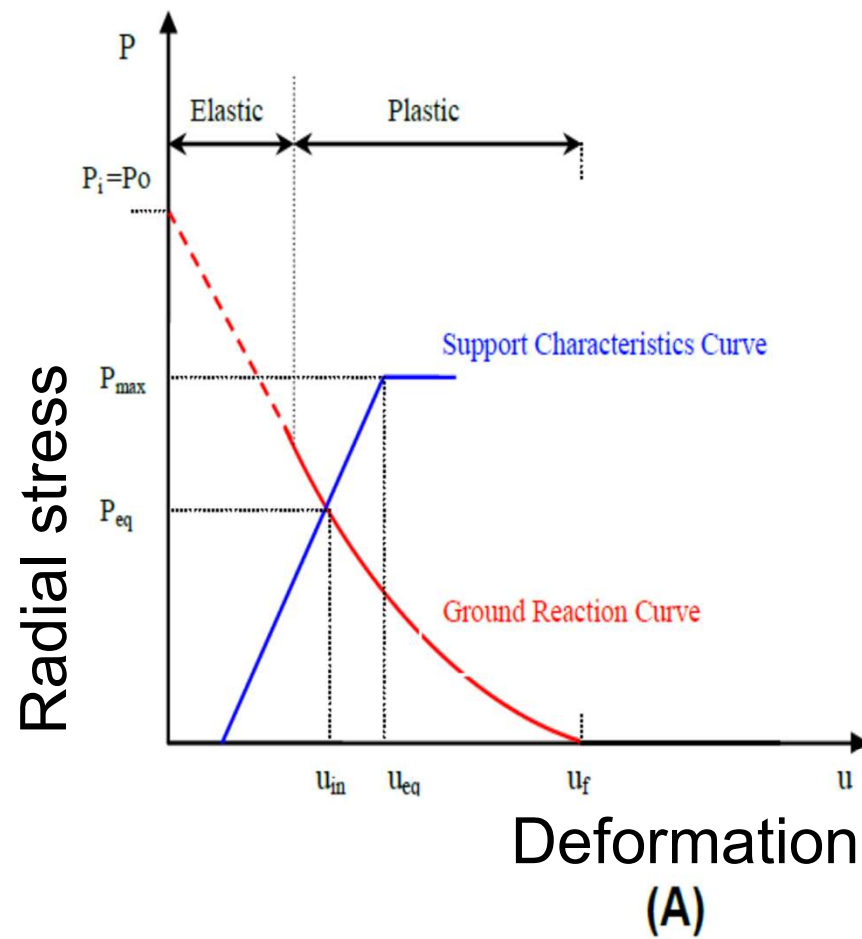
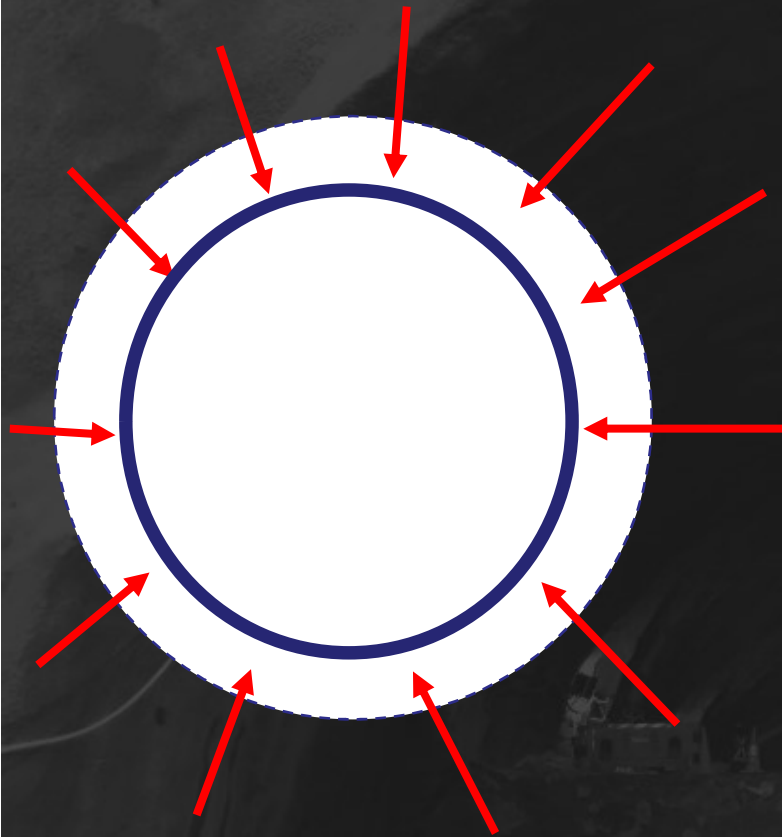
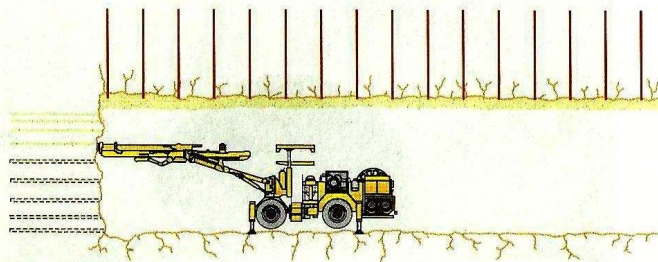


Figure 7-2: (A) The convergence-confinement method (B) Support characteristics curve (Hoek & Brown, 1980)

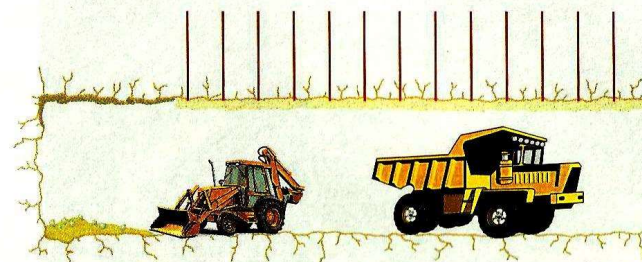


To allow that the rock take the load or part of the load a displacement of the tunnel periphery is required .

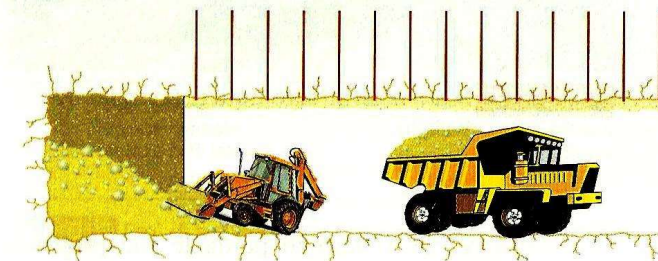
Primary support i.e. Shocrete rock bolts lattice girders have the only purpose to support the excavation phase (short term) and maintain the shape of the excavated profile .



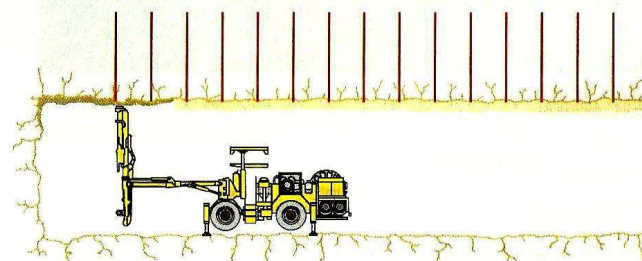
1. Perforazione e carica della volata



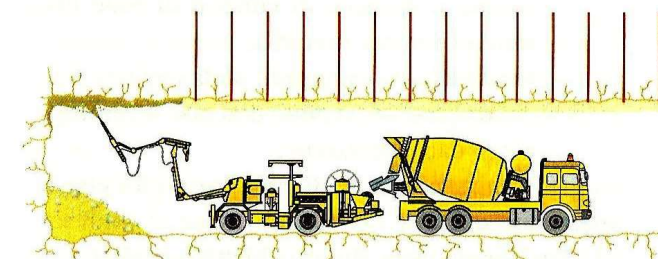
4. Completamento della rimozione dello smarino



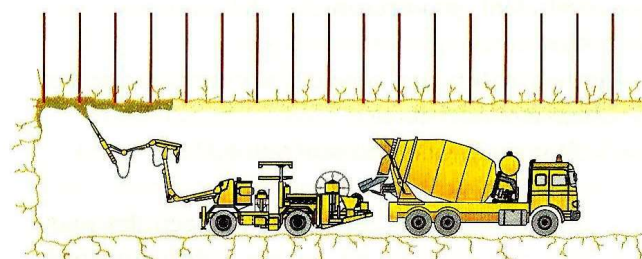
2. Disgaggio e rimozione dello smarino



5. Sostegno mediante bulloni



3. Protezione del fronte con gunite



6. Sostegno mediante calcestruzzo proiettato

NATM construction method



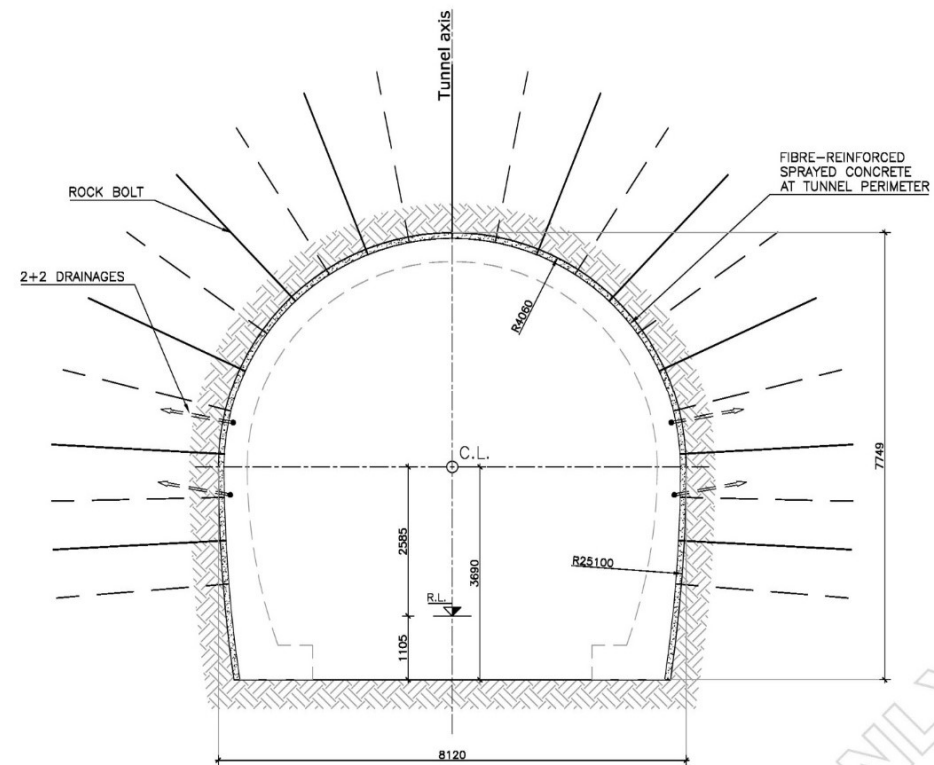
Blasting

BLASTING
MINING
UNDERGROUND

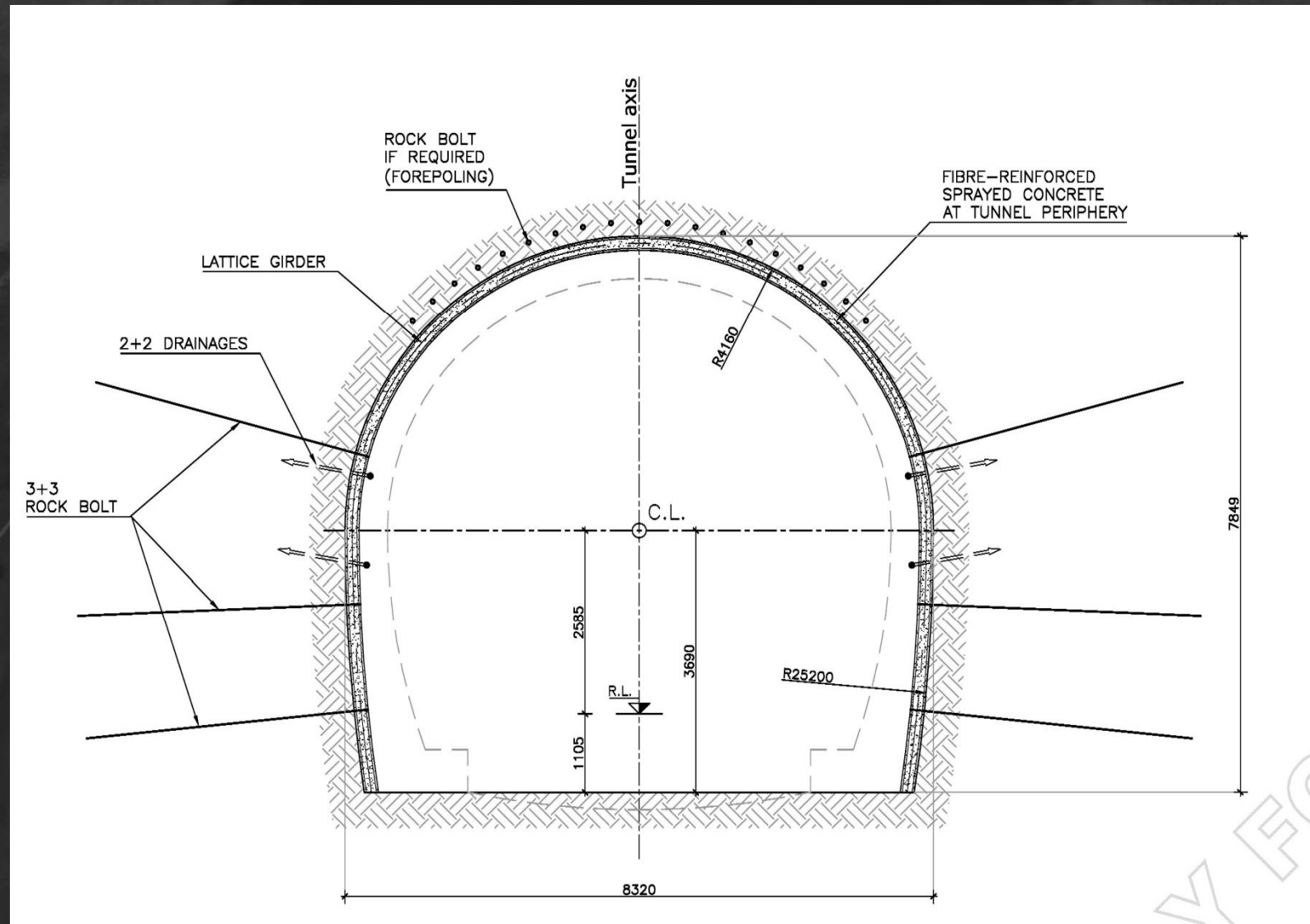
Waterproofing and final lining

TECHNOFLICKS 2011

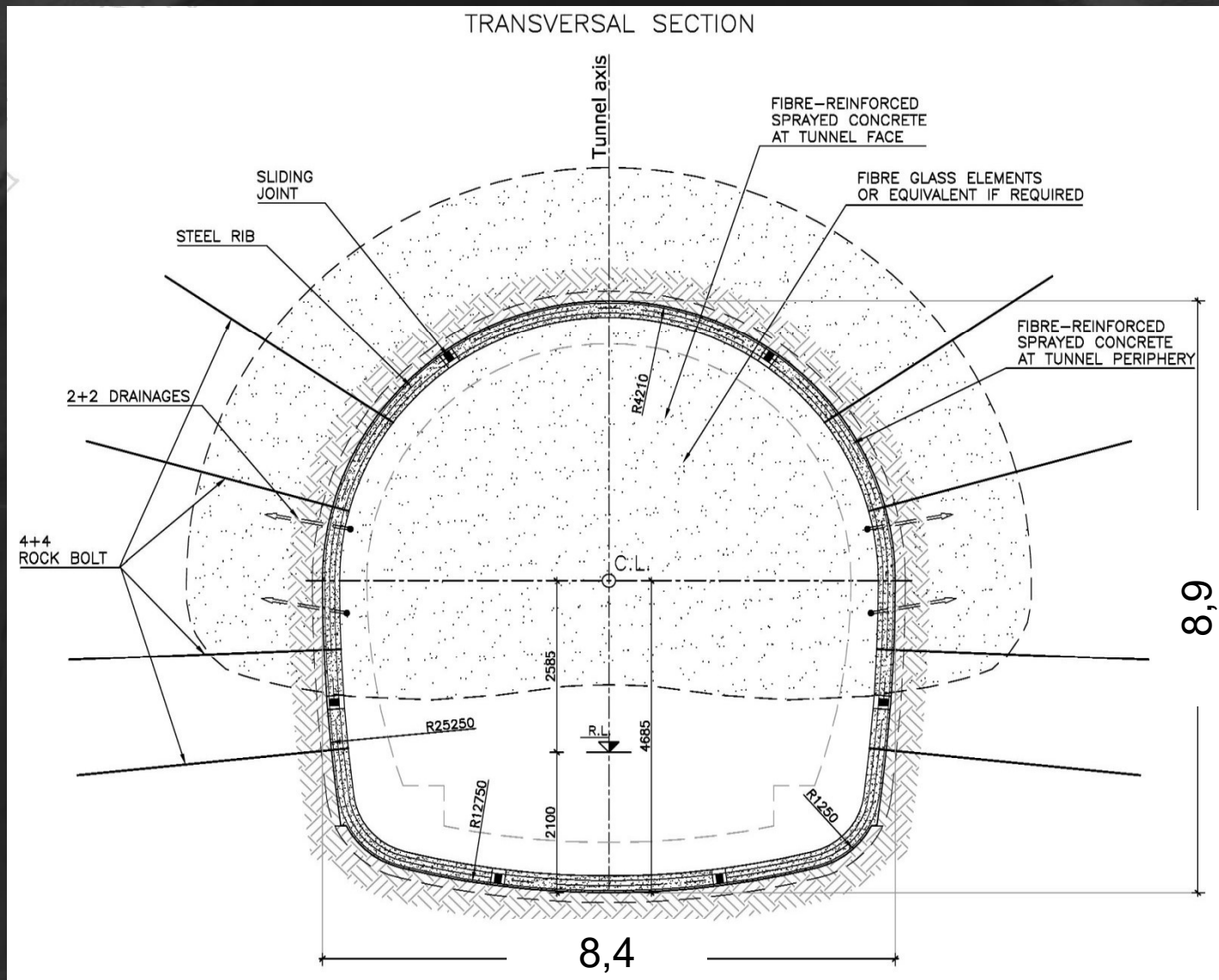
Support type



Support type



Support type



ARY INVERT
WIRE MESH
EEL FIBRES)

SHOTCRETE AT TUNNEL FACE

PIPE ROOF

SHOTCRETE REINFORCED
OR WITH STEEL FIBRES

SHOTCRETE AT TUNNEL FACE

ROCK BOLTS
34880

4.54°

11320

6924

31184

4430

5059

10274

31185

808

1132

3121

650

3121

5237

2652

37145

3051

TRACK

RAIL LEVEL ±0.000

SUPPORT CLASS F

STEEL RIBS (I-PROFILE)

DRAINAGE/EXPLORA
BORE HOLES

FACE ROCK BOL
(FULLY INJECTE

TEMPORARY
(SHOTCRETE
OR WITH ST

DRAINAGE/EXPLORA
BORE HOLES

Pure NATM state that primary support is enough to support the tunnel load

Chenani Nashri concession agreement based on «pure» NATM

SECTION 7 - INNER LINING CONCRETE

7.1 GENERAL

This section contains specifications for the construction of the final tunnel lining, the foundation beams and the invert arch. These structures are predominantly unreinforced, but they may also be reinforced locally, as approved by the ENGINEER.

7.1.1 Description

- a. The final tunnel lining, a cast-in-situ concrete lining increases the safety factor of the tunnel lining system, provides a uniform interior surface and improves the water tightness of the tunnel lining. A smooth interior surface is required for air flow, aesthetic, lighting and maintenance reasons.



Primary support is made by :

-Shotcrete

-Bolts

-Latticegirders or H beams

-Pipe roof

Short and long term support ?

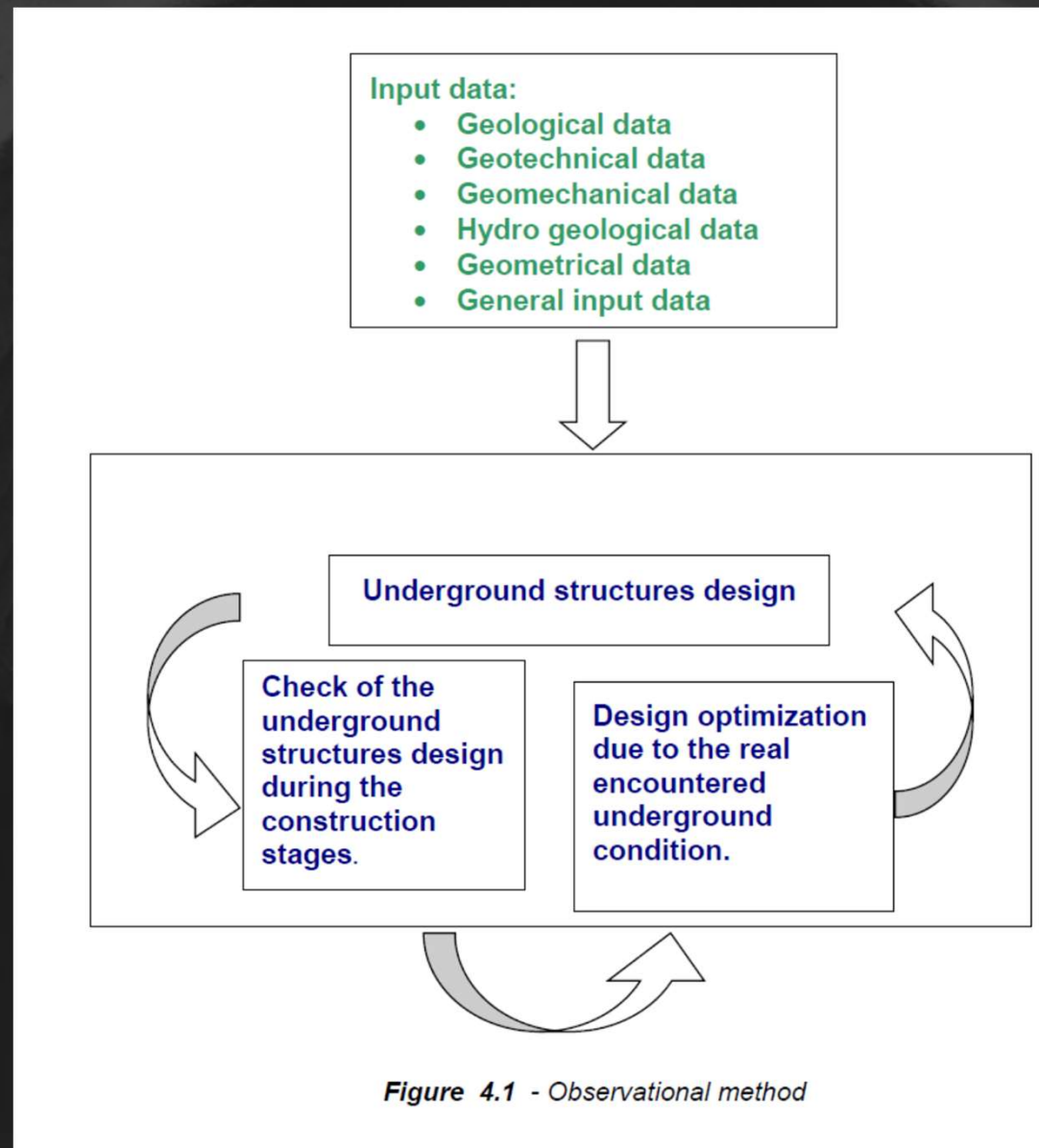


Figure 4.1 - Observational method

Load acting on the final lining

Empirical, analytical and **numerical** methods are used to estimate the ground load acting

elastic behaviour (“a/b” and “c” classes)

☐ **Empirical method:** the RMi system (Palmström 1996, 2000) or Q-Barton System (Grimstad & Barton, 1985).

elasto-plastic behaviour with relevant plastic zone around the tunnel (ex: deep tunnel, “d” classes):

☐ **Analytical method:** Convergence-Confinement Method (Carranza-Torres 2004)

- Qualification of the effect of the radial bolting according to the concept of “effective cohesion” (Grasso et al., 1989a,b).

Load acting on the final lining

- In case of **elastic behaviour**, the equations proposed by Unal (1983, 1992) is used to estimate the permanent support pressure (rock load):

$$p_v = \frac{100 - \text{RMR}}{100} \cdot \gamma \cdot B$$

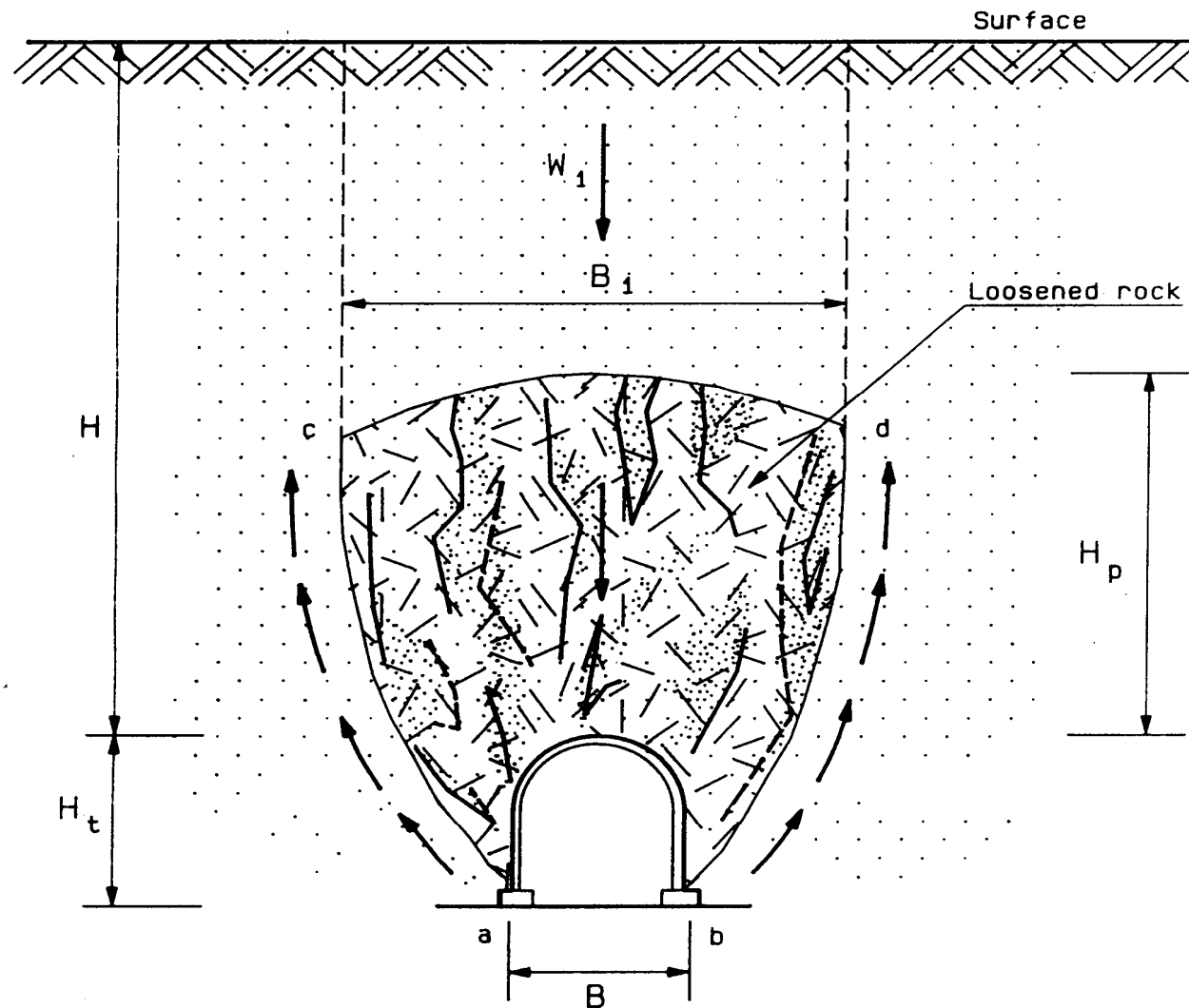
$$p_v = \frac{100 - \text{RMR}}{100} \cdot \gamma \cdot B$$

where RMR is Rock Mass Rating and B is the horizontal span of the tunnel.

In the case of elasto-plastic behaviour:

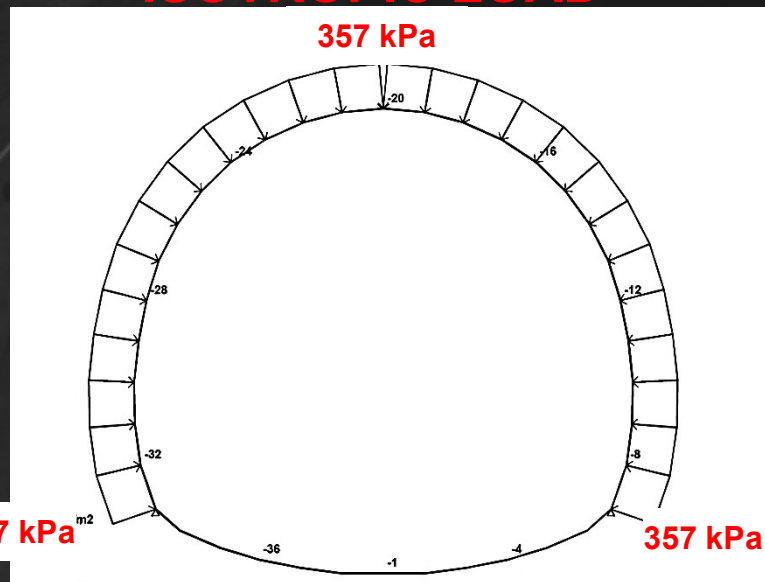
- for deep tunnel: convergence-confinement method
- for shallow tunnel: Terzaghi's formulation
- FINAL LINING CAN BE POURED WHEN MONTHLY DISPLACEMENT IS UNDER 2/4 MM (0,1 MM/DAY)

Load on shallow Tunnel Terzaghi 1946

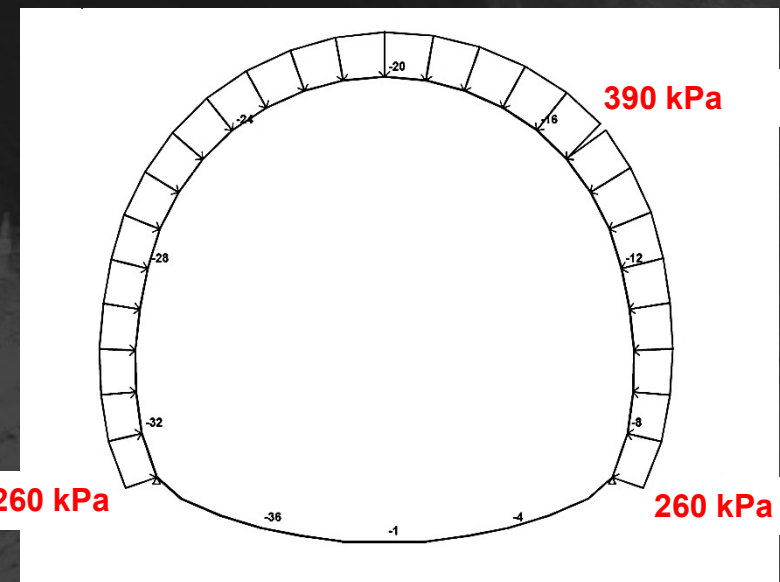


Load				
Load Condition	Type	$P_{(\theta = -135^\circ)}$ (kPa)	K_0 (-)	$P_{(\theta = 45^\circ)}$ (kPa)
Isotropic	$\gamma \cdot (R_{pl} - R_0)(*)$	357	1.0	357
Anisotropic	$\gamma \cdot (R_{pl} - R_0)(*)$	260	1.5	390

ISOTROPIC LOAD



ANISOTROPIC LOAD





Conclusion

Design and calculation of tunnel
aren't defined by standard

Multi criteria approach is the most
reliable solution

BUT NATM IS NOT THE ONLY WAY

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